

## Three-phase Brushless Motor PWM Controller with Digital Speed Control

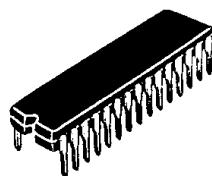
### Description

HA13484/NT are PWM control IC for general use three-phase brushless DC motor and have following functions and features.

### Functions

- Three-phase commutation circuit
- PWM control system
- Digital speed control system
- FG amp
- CLK oscillator
- Ready
- Direction
- Chip enable
- Current limiter
- Hall amps input dis-connection protect
- Low voltage inhibit

HA13484NT



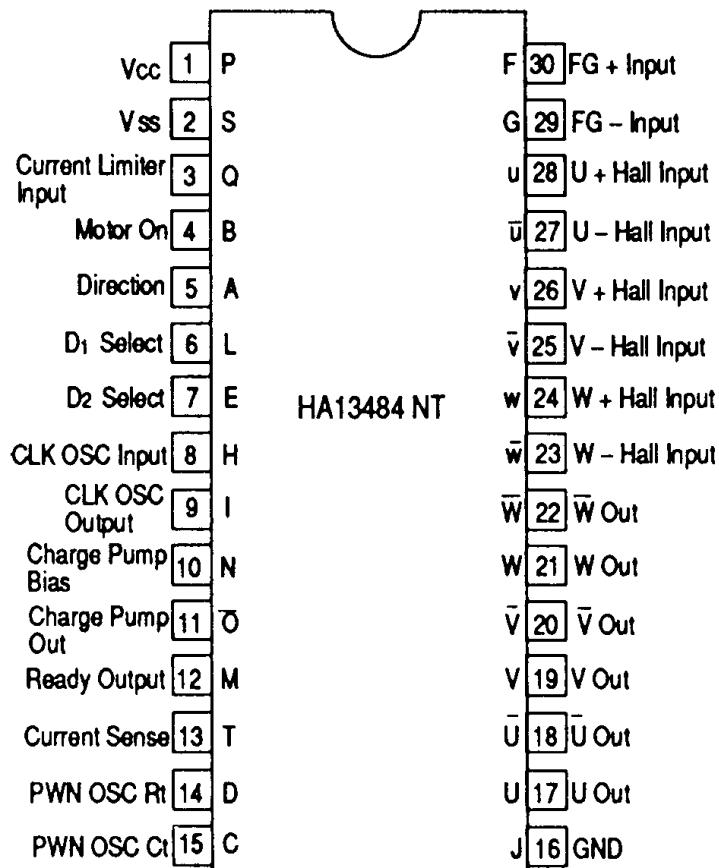
(DP-30S)

### Features

- Wide operating voltage range  
4.25 to 24.5 V
- Can handle various CLK frequency
- Can adjust limiting current by DC input

### Ordering Information

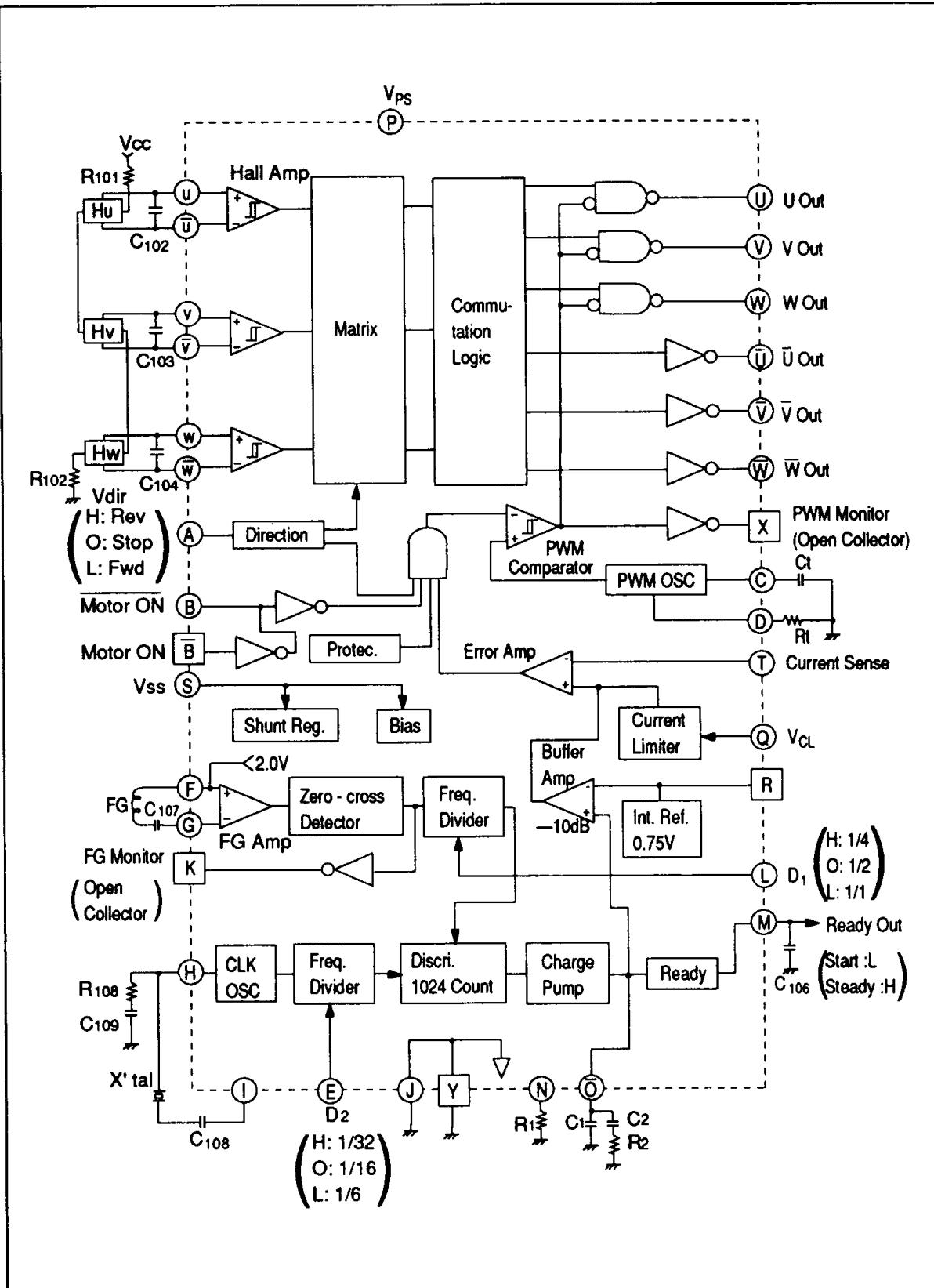
Type No.	Package
HA13484NT	400mil 30pin plastic shrink DIP (DP-30S)

**Pin Arrangement**

(Top View)



## Block Diagram



# HA13484NT

**Table 1 External Components**

Parts No.	Recommended value	Purpose	Note
R <sub>101</sub> , R <sub>102</sub>	—	Hall elements bias	1
R <sub>103</sub> , R <sub>203</sub> , R <sub>303</sub>	—	For speed up	
R <sub>104</sub> , R <sub>204</sub> , R <sub>304</sub>	—	For limiting sink current	2
R <sub>105</sub> , R <sub>205</sub> , R <sub>305</sub>	—	For limiting sink current	2
R <sub>106</sub>		For stability	
R <sub>107</sub>	—	Bias for regulator	3
R <sub>108</sub>	470 Ω	OSC stability	4
R <sub>1</sub> , R <sub>2</sub>	—	Integral constant	5
R <sub>t</sub>	6.8 kΩ	Time constant for PWM OSC	6
R <sub>NF</sub>	—	Current sense	7
C <sub>101</sub> , C <sub>102</sub> , C <sub>103</sub>	0.047 μF	For stability	
C <sub>104</sub>	≥0.1 μF	Vcc by-passing	
C <sub>105</sub>		For stability	
C <sub>106</sub>	1.0 μF	Filter for ready	
C <sub>107</sub>	1.0 μF	FG coupling	8
C <sub>108</sub>	10 pF	AC coupling for OSC	
C <sub>109</sub>	4700 pF	OSC stability	4
C <sub>1</sub> , C <sub>2</sub>	—	Integral constant	5
C <sub>t</sub>	2200 pF	Time constant for PWM OSC	6
Q <sub>1</sub> , Q <sub>2</sub> , Q <sub>3</sub>	—	Source output transistor	
Q <sub>4</sub> , Q <sub>5</sub> , Q <sub>6</sub>	—	Sink output transistor	
D <sub>1</sub> , D <sub>2</sub> , D <sub>3</sub> , D <sub>4</sub> , D <sub>5</sub> , D <sub>6</sub>	—	Clamp diode	
X'tal	—	Reference resonator	9



Notes: 1. Set  $R_{101}$ ,  $R_{102}$  in order to get hall element output more than 100 mVPP.

2.  $R_{x04}$  and  $R_{x05}$  should be designed as

$$R_{x04}(k\Omega) \geq \frac{V_{cc}(V) - V_{BE}(V)}{20}, \quad R_{x05}(k\Omega) \geq \frac{V_{cc}(V)}{20}$$

Where  $V_{BE}$  is the base-emitter voltage of  $Q_1$  to  $Q_3$ .

3.  $R_{107}$  should satisfy the following equation.

$$\frac{V_{cc \ max}(V) - 6.3}{0.06} \leq R_{107}(\Omega) \leq \frac{V_{cc \ min}(V) - 6.3}{0.03}$$

**Table 3 Absolute Maximum Ratings ( $T_a = 25^\circ C$ )**

Item	Symbol	Rating	Unit	Note
Supply voltage	$V_{PS}$	34.5	V	1
Input voltage	$V_{in}$	0 to $V_{SS}$	V	2
Output current	$I_{out}$	30	mA	
$V_{SS}$ input current	$I_{SS}$	60	mA	
Power dissipation	$P_T$	650	mW	
Operating temperature range	$T_{opr}$	-20 to +70	°C	
Storage temperature range	$T_{stg}$	-55 to +125	°C	

The absolute maximum ratings are limiting values, to be applied individually, beyond which the device may be permanently damaged. Functional operation under any of these conditions is not guaranteed. Exposing a circuit to its absolute maximum rating for extended periods of time may affect the device's reliability.

Notes: 1. Recommended operating voltage range as follows.

$$V_{PS} = 4.25 \text{ to } 34.5 \text{ V}$$

$$V_{SS} = 4.25 \text{ to } V_{reg}$$

2. Apply to pin A, B,  $\bar{B}$ , E, L and T.

**Table 4 Electrical Characteristics ( $T_a = 25^\circ C$ ,  $V_{PS} = 24 \text{ V}$ ,  $V_{SS} = 5.0 \text{ V}$ )**

Item	Symbol	Min	Typ	Max	Unit	Test conditions	Applica- tion terminal	Note
Supply current	$I_{PS}$	—	2.5	4.0	mA	$V_{PS} = 34.5 \text{ V}$	P	
	$I_{SS}$	—	20	30	mA	$V_{SS} = 6.0 \text{ V}$	S	
Shunt reg.	Reg. voltage	$V_{reg}$	6.0	6.5	V	$I_{SS} = 30 \text{ to } 60 \text{ mA}$	S	1
	Operating resistance	$R_d$	—	—	$\Omega$	$I_{SS} = 30 \text{ to } 60 \text{ mA}$		



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## Electrical Characteristics ( $T_a = 25^\circ\text{C}$ , $V_{PS} = 24\text{ V}$ , $V_{SS} = 5.0\text{ V}$ ) (cont)

Motor ON & Motor ON	Input low voltage	$V_{IL1}$	—	—	0.8	V	$B, \bar{B}$
	Input high voltage	$V_{IH1}$	2.0	—	—	V	
	Input current	$I_{L1}$	—	—	$\pm 10$	$\mu\text{A}$	
		$I_{IL1}$	—	60	200	$\mu\text{A}$	$V_{in} = 0\text{ V}$
		$I_{IH1}$	—	—	$\pm 10$	$\mu\text{A}$	$V_{in} = V_{SS}$
Direction $D_1$ & $D_2$	Input low voltage	$V_{IL2}$	—	—	1.0	V	$A, E, L$
	Input middle voltage	$V_{IM2}$	1.75	—	2.75	V	
	Input high voltage	$V_{IH2}$	3.5	—	—	V	
	Input current	$I_2$	—	—	$\pm 10$	$\mu\text{A}$	
Hall amp	Input common mode voltage range	$V_H$	2.1	—	$V_{PS}$	V	$U, \bar{U},$ $V, \bar{V},$ $W, \bar{W}$
	Hysteresis	$HYS_H$	—	20	—	mV	
	Input current	$I_H$	—	—	$\pm 15$	$\mu\text{A}$	
Output	Leak current	$I_{CER}$	—	—	100	$\mu\text{A}$	$U, \bar{U},$ $V, \bar{V},$ $W, \bar{W}$
	Saturation voltage	$V_{sat}$	—	—	0.4	V	
	Transition time	$t_{PHL}$	—	0.25	—	$\mu\text{s}$	
		$t_{PLH}$	—	0.3	—	$\mu\text{s}$	turn-off
PWM OSC	Rt bias voltage	$V_{Rt}$	—	1.25	—	V	D
	Operating frequency range	$f_p$	5	—	100	kHz	
	Amplitude	A	—	2.0	—	$V_{PP}$	
Error amp	input current	$I_{er}$	—	—	$\pm 5$	$\mu\text{A}$	$V_i = 0$ to $1.0\text{ V}$
Buffer amp	Int. ref. voltage	$V_{ref1}$	—	0.75	—	V	R
	Voltage gain	$G_{d1}$	—	-10	—	dB	
					Pin 0 to T		T



**Electrical Characteristics (Ta = 25 °C, V<sub>PS</sub> = 24 V, V<sub>SS</sub> = 5.0 V) (cont)**

Current limiter	Input current	I <sub>CL</sub>	—	±5	μA	V <sub>CL</sub> = 0 to V <sub>SS</sub>	Q
	Offset voltage	V <sub>OS</sub>	-10	-25	-40	mV	V <sub>CL</sub> = 0 to 1.0 V
Charge Pump	R <sub>1</sub> bias voltage	V <sub>R1</sub>	—	1.25	—	V	R <sub>1</sub> = 15 kΩ
	Charge current	I <sub>CHA</sub>	—	$\frac{VR_1}{4R_1}$	—	A	R <sub>1</sub> = 15 kΩ
	Discharge current	I <sub>DIS</sub>	—	$-\frac{VR_1}{4R_1}$	—	A	R <sub>1</sub> = 15 kΩ
	Leak current	I <sub>OFF</sub>	—	—	±50	nA	
FG amp	Input bias voltage	V <sub>FG</sub>	—	1.95	—	V	F
	Input resistance	R <sub>FG</sub>	—	800	—	Ω	F, G
	Input voltage range	V <sub>INFG</sub>	8	—	50	mV <sub>PP</sub>	
	Noise margin	nd	—	—	2	mV <sub>PP</sub>	Differential noise
		nc	—	—	1.0	V <sub>PP</sub>	Common mode noise
CLK OSC	Maximum frequency	f <sub>C</sub>	—	—	8.0	MHz	I
Discr	Count number	N	—	1024	—	—	—
Ready	Input threshold voltage	V <sub>IL3</sub>	—	V <sub>ref1</sub>	—	V	O 3
		V <sub>IH3</sub>	—	V <sub>ref1</sub> + 3V <sub>CL</sub>	—	V	
	Output current	I <sub>R+</sub>	—	300	—	μA	V <sub>out</sub> = 2 V Source M
		I <sub>R-</sub>	—	-300	—	μA	Sink
	Output low voltage	V <sub>OL3</sub>	—	—	0.4	V	
	Output high voltage	V <sub>OH3</sub>	4.5	5.0	5.5	V	
PWM & FG monitor	Leak current	I <sub>CER4</sub>	—	—	±10	μA	V <sub>out</sub> = 34.5 V K, X
	Output low voltage	V <sub>OL4</sub>	—	—	0.4	V	I <sub>out</sub> = 1.0 mA
Protect	LVI threshold	V <sub>SD</sub>	—	3.75	—	V	S



## HA13484NT

Notes: 1. See Figure 1. And Rd can be calculated as:

$$Rd(\Omega) = 33.3 \Delta V_{reg}(V)$$

2. See Timing chart.

3. See Figure 2.

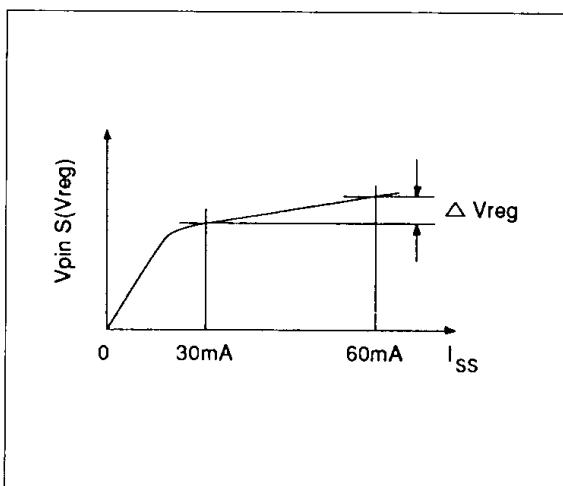


Figure 1.

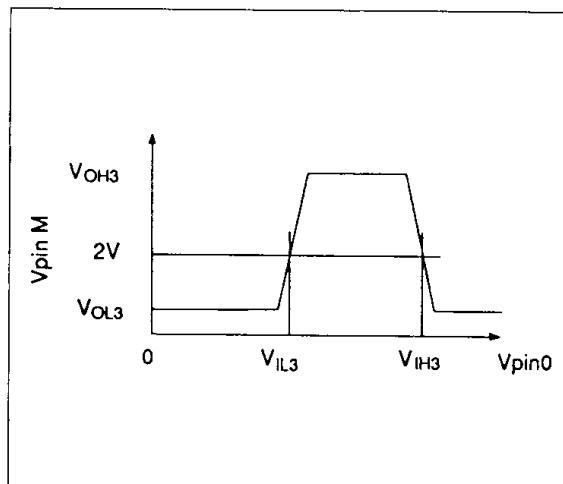


Figure 2.

4. Not necessary if the CLK frequency is less than 4MHz.

5. The integral constant can be designed as

$$\omega_0 \leq \frac{2\pi f_{FG} D_1}{20} \quad (\text{rad/s})$$

$$R_2 = \frac{4}{R_1} \cdot \frac{\omega_0 R_{NF} N_o J}{9.55 \cdot V_{R1} G_{ctl} K_T}$$

$$R_1 \leq 30(\text{k}\Omega)$$

$$C_1 = \frac{1}{\sqrt{10} \omega_0 R_2} \quad (\text{F})$$

$$C_2 = 10C_1 \quad (\text{F})$$

Where

$\omega_0$ =Servo loop's time constant

$f_{FG}$ =FG frequency (Hz)

$D_1$ =Frequency divider ratio

$R_{NF}$ =Current sense resistor ( $\Omega$ )

$N_o$ =Rotation number (rpm)

$V_{R1}$ =Charge pump reference voltage, 1.25 V

$G_{ctl}$ =Control gain, 0.316

$J$ =Inertia moment ( $\text{kg}\cdot\text{cm}\cdot\text{s}^2$ )

$K_T$ =Torque constant ( $\text{kg}\cdot\text{cm}/\text{A}$ )

6. The PWM frequency  $f_p$  can be calculated as

$$f_p = \frac{V_{Rt}}{8Ct R_t} \quad (\text{Hz})$$

Where  $V_{Rt}$  is the  $R_t$  reference voltage, 1.25 (V).

7. The limiting current  $I_{max}$  will be

$$I_{max} = \frac{V_{CL}(V)}{R_{NF}(\Omega)} \quad (\text{A})$$

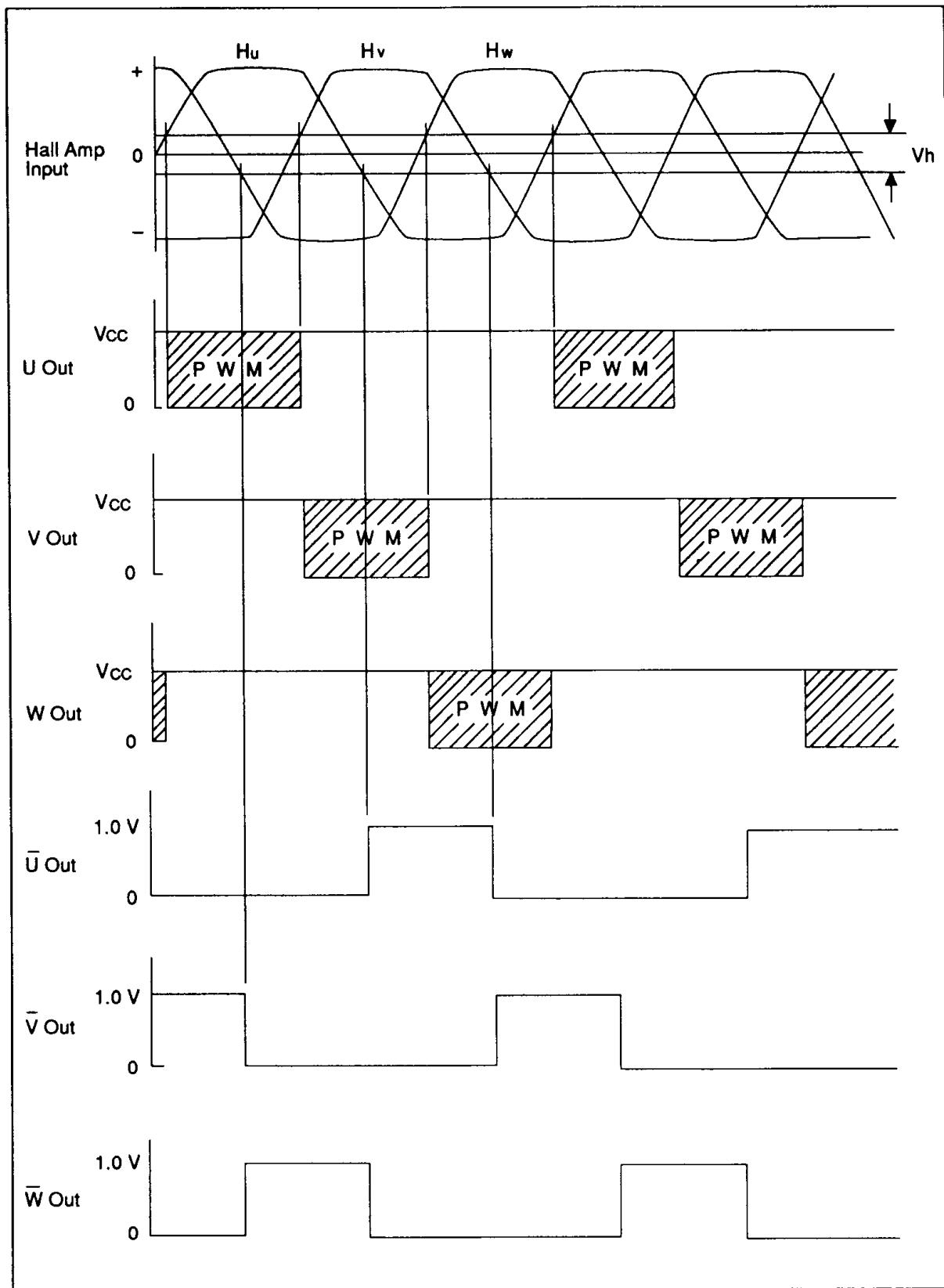
8.  $C_{107}$  can be designed using the following equation as an guide line.

$$C_{107} \geq \frac{1}{2500 f_{FG}} \quad (\text{F})$$

9. The relationship between FG frequency and X'tal frequency is as follows.

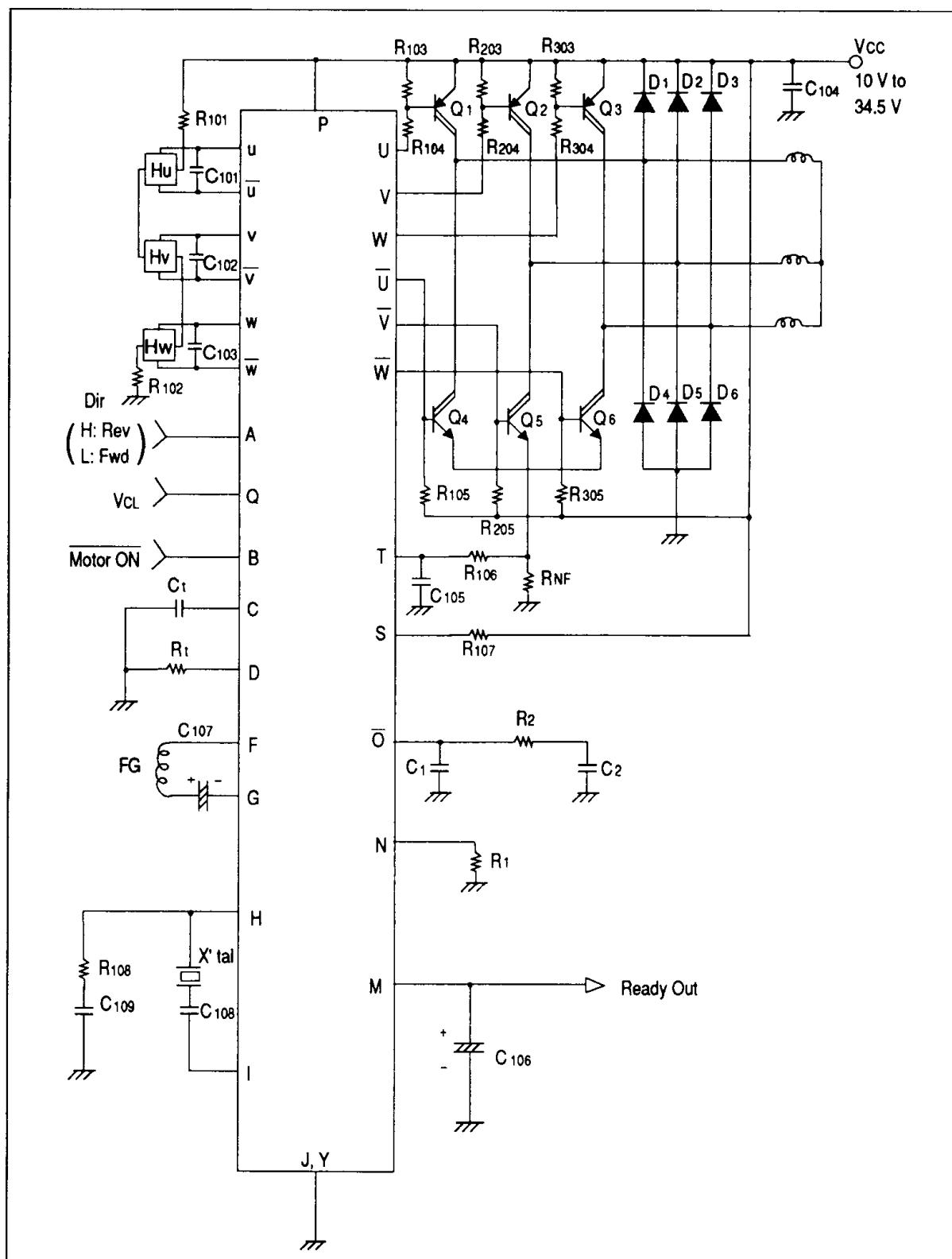
$$X'\text{tal} = \frac{8188 D_1 f_{FG}}{D_2} \quad (\text{Hz})$$

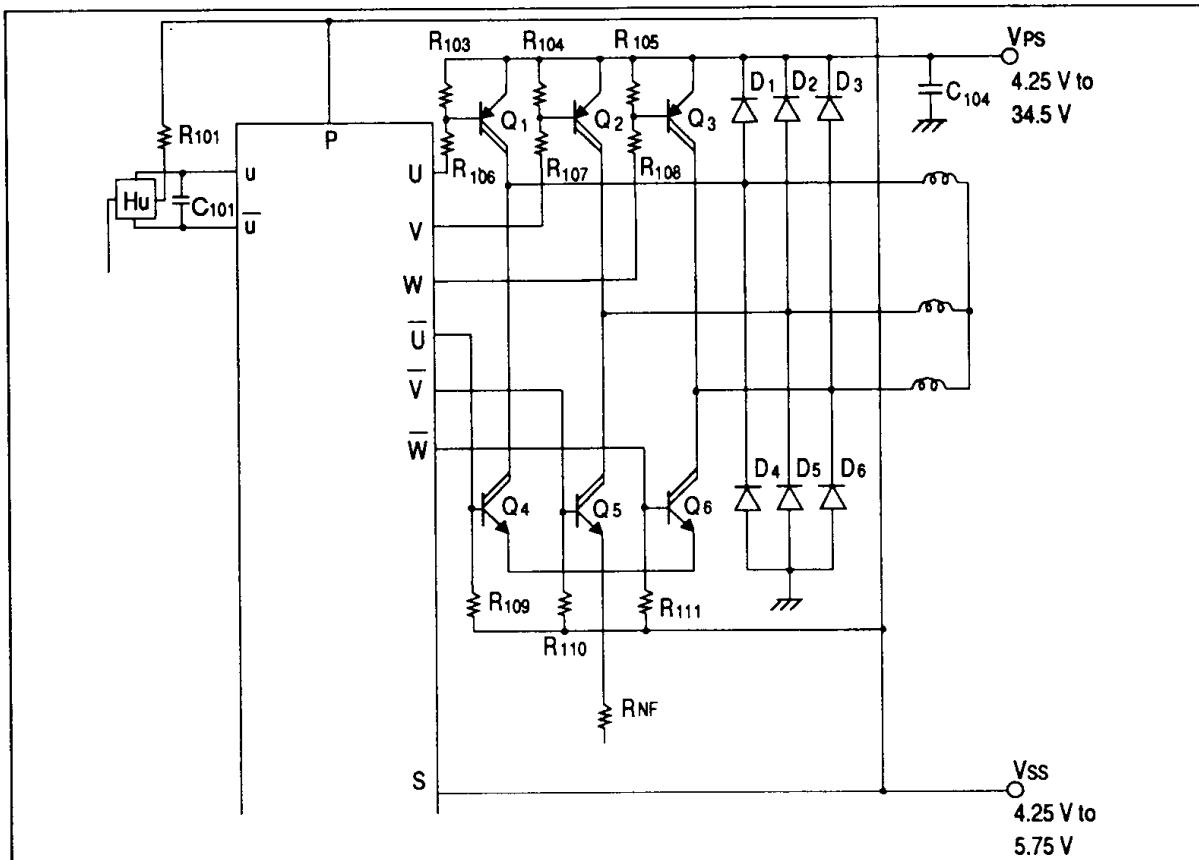
Where  $D_1$  and  $D_2$  are frequency divider ratio.

**Timing Chart**
**HITACHI**

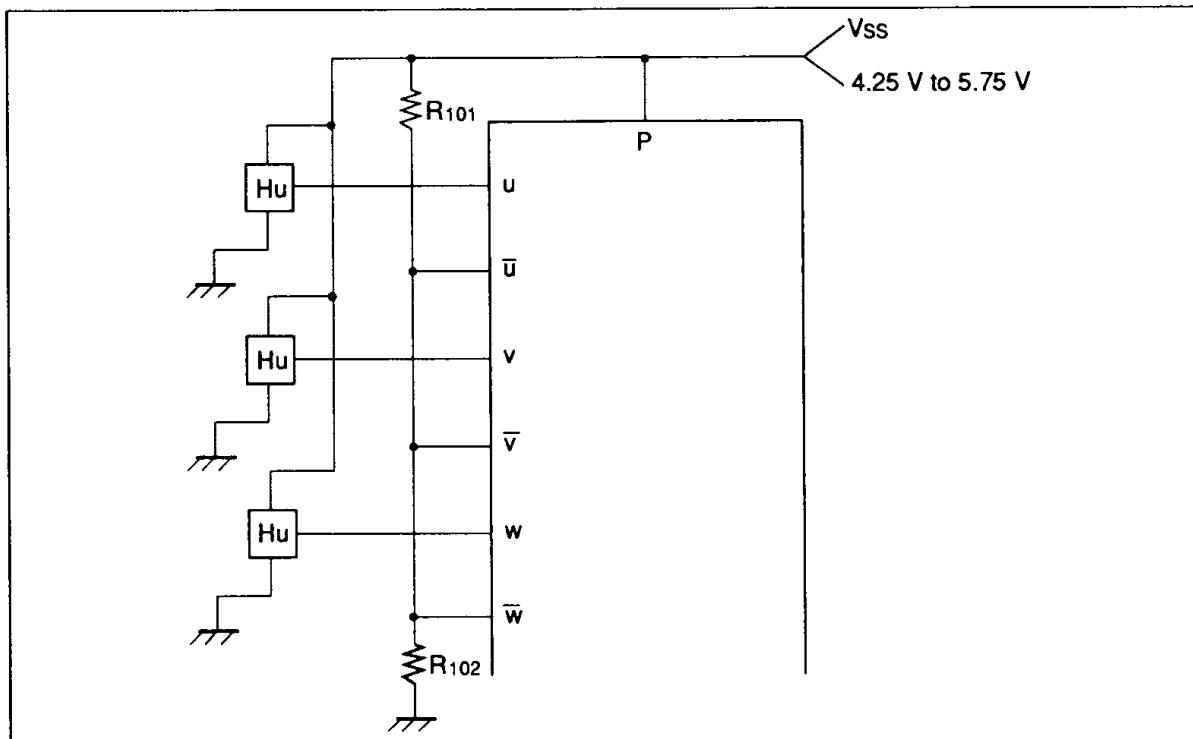
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**Application****Single Supply**
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Dual Supply



For Hall IC

