

FEATURES

- Low offset voltage and offset current
- Low offset voltage and current drift
- Low input bias current
- Low input noise voltage
- Large common mode and differential voltage ranges

ABSOLUTE MAXIMUM RATINGS

Supply Voltage	$\pm 22V$
Internal Power Dissipation (Note 1)	
Metal Can	500mW
Differential Input Voltage	$\pm 30V$
Input Voltage (Note 2)	$\pm 15V$
Storage Temperature Range	-65°C to +150°C
Operating Temperature Range (HC)	0°C to 70°C (HM) ... -55°C to +125°C
Lead Temperature (Soldering, 10s)	300°C 260°C
Output Short Circuit Duration (Note 3)	Indefinite

Note 1: Rating applies to ambient temperatures up to 70°C. Above 70°C ambient derate linearly at 6.3mW/°C for Metal Can, 8.3mW/°C for the DIP, and 5.6mW/°C for the Mini DIP.

Note 2. For supply voltages less than $\pm 15V$, the absolute maximum input voltage is equal to the supply voltage.

Note 3. Short Circuit may be to ground or either supply. Rating applies to +125°C case temperature or +75°C ambient temperature for $I_{SET} \leq 30\mu A$.

ORDERING INFORMATION

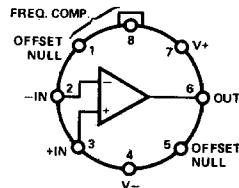
	Dice	TO-99 Can
μ A777C	μ A777C/D	μ A777HC
μ A777M	μ A777M/D	μ A777MC

GENERAL DESCRIPTION

The μ A777 is a monolithic Precision Operational Amplifier. It is an excellent choice when performance versus cost trade-offs are possible between super beta or FET input operational amplifiers and low cost general purpose operational amplifiers. Low offset and bias currents improve system accuracy when used in applications such as long term integrators, sample and hold circuits and high source impedance summing amplifiers. Even though the input bias current is extremely low, the μ A777 maintains full $\pm 30V$ differential voltage range. High common mode input voltage range, latch-up protection, short circuit protection and simple frequency compensation make the device versatile and easily used.

PIN CONFIGURATION

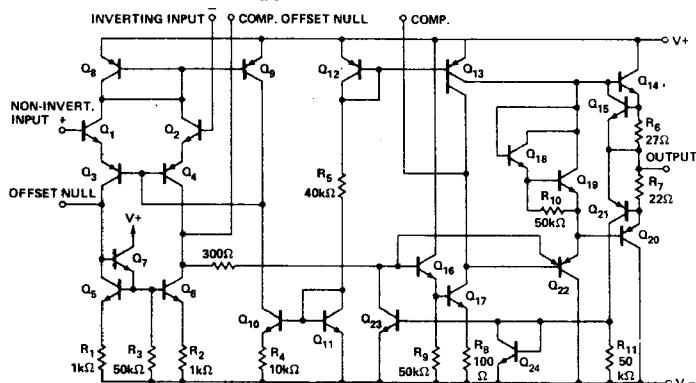
8-LEAD METAL CAN
(TOP VIEW)

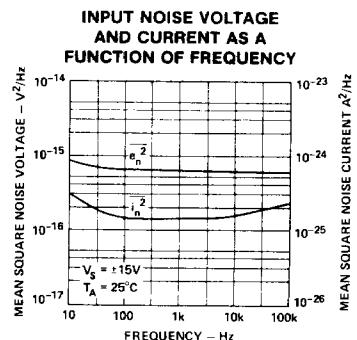
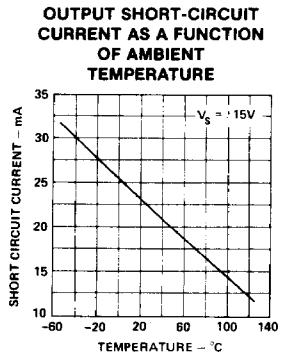
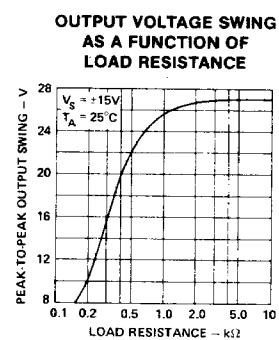
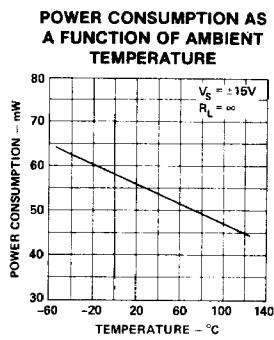
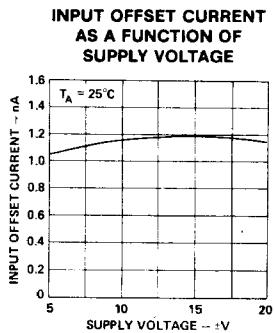
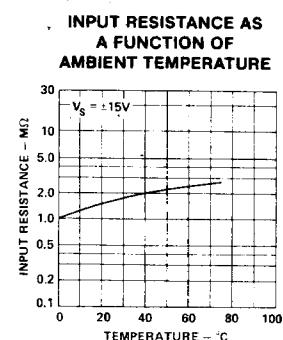
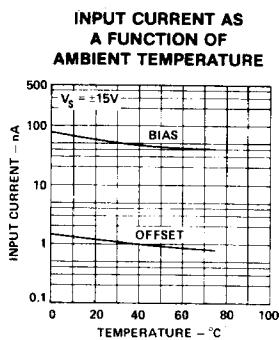
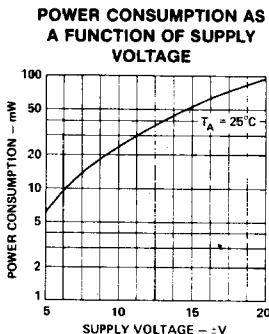
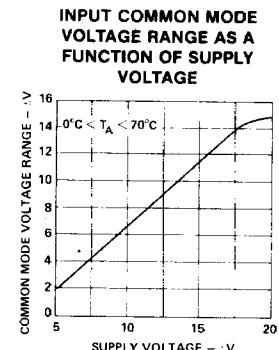
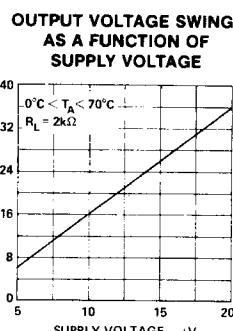
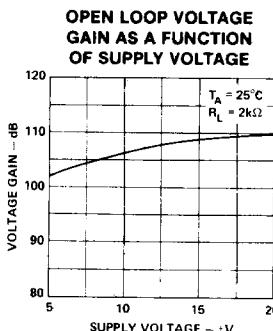


(outline dwg TY)

ELECTRICAL CHARACTERISTICS FOR μ A777 ($V_s = \pm 15V$, $T_A = 25^\circ C$, $C_C = 30pF$ unless otherwise specified)

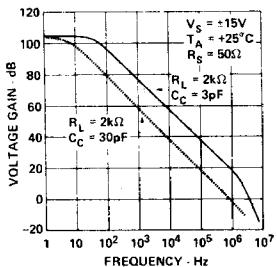
PARAMETERS		CONDITIONS	MIN	TYP	MAX	UNITS
Input Offset Voltage		$R_S \leq 50k\Omega$		0.7	5.0	mV
Input Offset Current				0.7	20.0	nA
Input Bias Current				25	100	nA
Input Resistance			1.0	2.0		M Ω
Input Capacitance				3.0		pF
Offset Voltage Adjustment Range				± 25		mV
Large Signal Voltage Gain		$R_L \geq 2k\Omega$, $V_{OUT} = \pm 10V$	25,000	250,000		V/V
Output Resistance				100		Ω
Output Short Circuit Current				± 25		mA
Supply Current				1.9	2.8	mA
Power Consumption				60	85	mW
Transient Response (Voltage Follower, Gain of 1)	Rise Time Overshoot	$V_{IN} = 20mV$, $C_C = 30pF$ $R_L = 2k\Omega$, $C_L \leq 100pF$		0.3		μ s
				5.0		%
Slew Rate (Voltage Follower, Gain of 1)		$R_L \geq 2k\Omega$		0.5		V/ μ s
Transient Response (Voltage Follower, Gain of 10)	Rise Time Overshoot	$V_{IN} = 20mV$, $C_C = 3.5pF$ $R_L = 2k\Omega$, $C_L \leq 100pF$		0.3		μ s
				5.0		%
Slew Rate (Voltage Follower, Gain of 10)		$R_L \leq 2k\Omega$, $C_C = 3.5pF$		5.5		V/ μ s
The following specifications apply over operating temperature range.						
Input Offset Voltage		$R_S \leq 50k\Omega$		0.8	5.0	mV
Average Input Offset Voltage Drift		$R_S \leq 50k\Omega$		4.0	30	μ V/ $^\circ$ C
Input Offset Current				40		nA
Average Input Offset Current Drift		$25^\circ C \leq T_A \leq +70^\circ C$ $0^\circ C \leq T_A \leq +25^\circ C$		0.01	10.3	nA/ $^\circ$ C
				0.02	0.6	nA/ $^\circ$ C
Input Bias Current					200	nA
Input Voltage Range			± 12	± 13		V
Common Mode Rejection Ratio		$R_S \leq 50k\Omega$	70	95		dB
Supply Voltage Rejection Ratio		$R_S \leq 50k\Omega$		15	150	μ V/V
Large Signal Voltage Gain		$R_L \geq 2k\Omega$, $V_{OUT} = \pm 10V$	15,000			V/V
Output Voltage Swing		$R_L \geq 10k\Omega$	± 12	± 14		V
		$R_L \geq 2k\Omega$	± 10	± 13		V
Power Consumption				60	100	mW

EQUIVALENT CIRCUIT

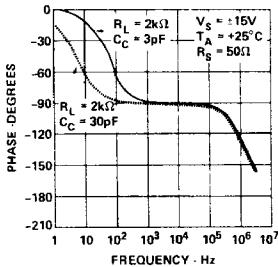
TYPICAL PERFORMANCE CURVES

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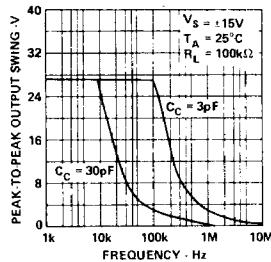
OPEN LOOP VOLTAGE GAIN AS A FUNCTION OF FREQUENCY



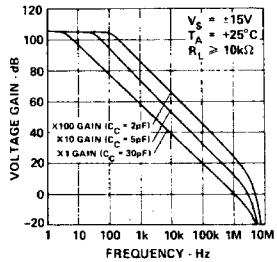
OPEN LOOP PHASE RESPONSE AS A FUNCTION OF FREQUENCY



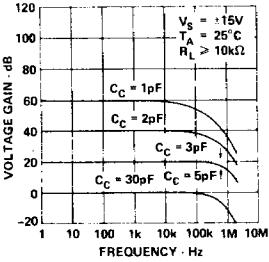
OUTPUT VOLTAGE SWING AS A FUNCTION OF FREQUENCY



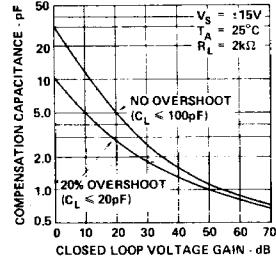
OPEN LOOP VOLTAGE GAIN AS A FUNCTION OF FREQUENCY FOR VARIOUS GAIN/COMPENSATION OPTIONS



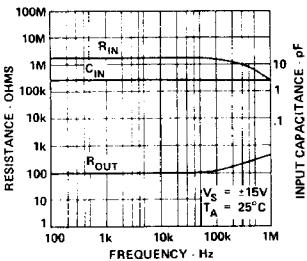
FREQUENCY RESPONSE FOR VARIOUS CLOSED-LOOP GAINS



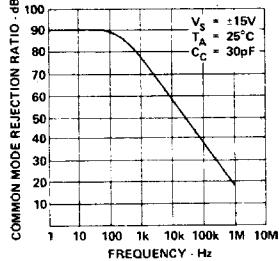
COMPENSATION CAPACITANCE AS A FUNCTION OF CLOSED LOOP VOLTAGE GAIN



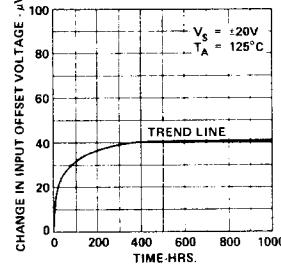
INPUT RESISTANCE, OUTPUT RESISTANCE, AND INPUT CAPACITANCE AS A FUNCTION OF FREQUENCY



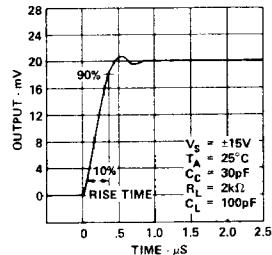
COMMON MODE REJECTION RATIO AS A FUNCTION OF FREQUENCY



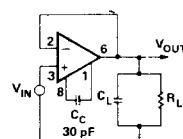
INPUT OFFSET VOLTAGE DRIFT AS A FUNCTION OF TIME



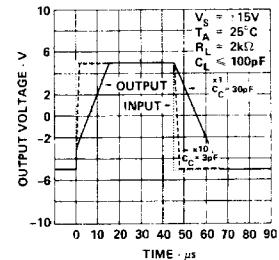
VOLTAGE FOLLOWER TRANSIENT RESPONSE (GAIN OF 1)



TRANSIENT RESPONSE TEST CIRCUIT

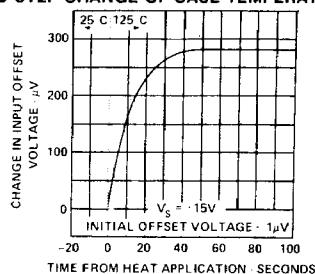


VOLTAGE FOLLOWER LARGE SIGNAL PULSE RESPONSE

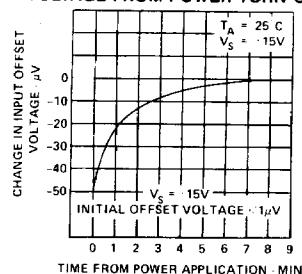


TYPICAL PERFORMANCE CURVES

**THERMAL RESPONSE OF INPUT OFFSET VOLTAGE
TO STEP CHANGE OF CASE TEMPERATURE**

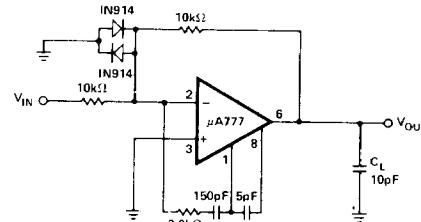
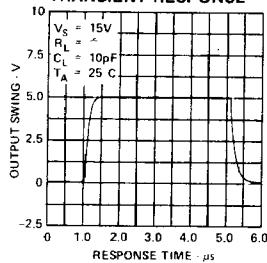


**STABILIZATION TIME OF INPUT OFF-SET
VOLTAGE FROM POWER TURN-ON**

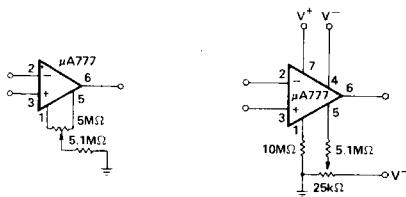


FEED FORWARD COMPENSATION

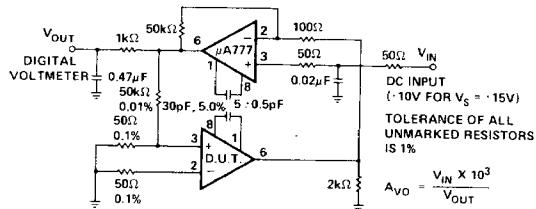
**LARGE SIGNAL FEEDFORWARD
TRANSIENT RESPONSE**



**VOLTAGE OFFSET
NULL CIRCUIT**



GAIN TEST CIRCUIT



SUGGESTED

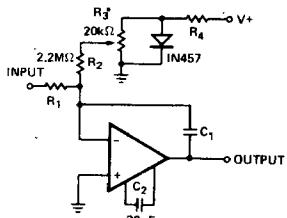
ALTERNATE

μA777

INTERSIL

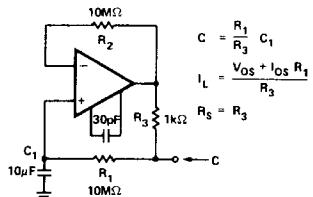
TYPICAL APPLICATIONS

BIAS COMPENSATED LONG TIME INTEGRATOR

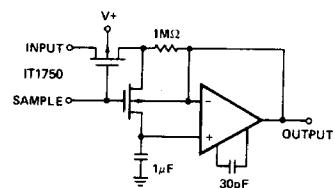


*ADJUST R_3 FOR MINIMUM INTEGRATOR DRIFT

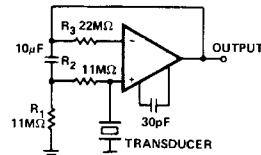
CAPACITANCE MULTIPLIER



SAMPLE AND HOLD



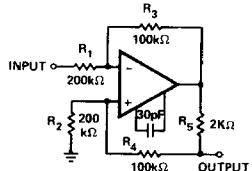
AMPLIFIER FOR CAPACITANCE TRANSDUCERS



LOW FREQUENCY CUTOFF $R_1 \times C_1$

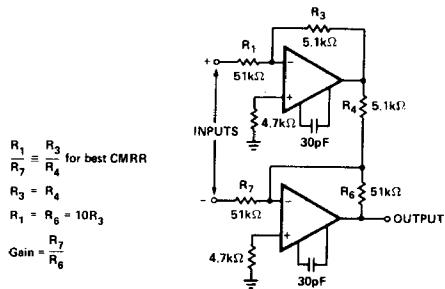
5

BILATERAL CURRENT SOURCE



$$I_{\text{OUT}} = \frac{R_3}{R_1 R_5} V_{\text{IN}} ; R_1 = R_2 ; R_3 = R_4 + R_5$$

±100V COMMON MODE RANGE INSTRUMENTATION AMPLIFIER



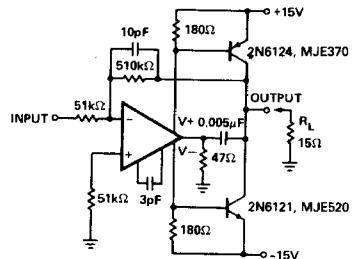
$$\frac{R_1}{R_7} = \frac{R_3}{R_4} \text{ for best CMRR}$$

$$R_3 = R_4$$

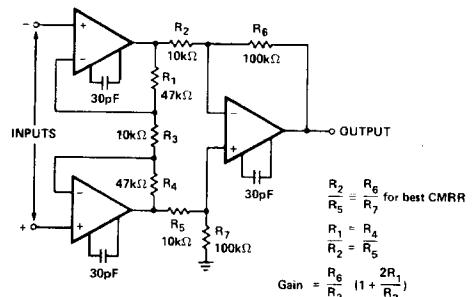
$$R_1 = R_6 = 10R_3$$

$$\text{Gain} = \frac{R_7}{R_6}$$

HIGH SLEW RATE POWER AMPLIFIER



INSTRUMENTATION AMPLIFIER WITH HIGH COMMON MODE REJECTION



$$\frac{R_2}{R_5} = \frac{R_6}{R_7} \text{ for best CMRR}$$

$$R_1 = R_4$$

$$R_2 = R_5$$

$$R_8 = R_9$$

$$\text{Gain} = \frac{R_6}{R_2} \left(1 + \frac{2R_1}{R_3} \right)$$